Switching Regulator IC Series

Bootstrap Circuit in the Buck Converter

This application note explains the step-up circuit using a bootstrap capacitor. In buck converters, this circuit is used when the high-side switch is the N-ch MOSFET.

1. Role of the bootstrap circuit in the buck converter

The configuration of the circuit in proximity to a buck converter depends on the polarity of the high-side switch.

When a P-ch MOSFET is used for the high-side switch, there are advantages over using a N-ch MOSFET, such as the capability of driving the switch with input voltage \( V_{IN} \) as the gate voltage, as well as voltage reduction and obtainment of the maximum duty. On the contrary, the use of a P-ch MOSFET requires a larger chip area for passing the same current.

The use of an N-ch MOSFET for the high-side switch requires a gate voltage of \( V_{IN} + V_{th} \) (threshold voltage of the N-ch MOSFET) or higher. A step-up circuit is required because the gate voltage is higher than \( V_{IN} \). This circuit is configured with an internal diode and an external bootstrap capacitor (charge pump type). The total cost, including the cost of the external bootstrap capacitor, can be lowered because the chip area can be reduced compared with the P-ch MOSFET, as mentioned above.

2. Description of the charge pump operation

In the charge-pump-type step-up circuit, the essential parts include a diode and a capacitor (bootstrap capacitor). The diode is often built-in as an element in the IC, and only the bootstrap capacitor is connected externally.

Figure 1 shows an example of an actual circuit.

The voltages on the SW and BOOT pins in the example of Figure 1 are described as shown in Figure 2, where \( V_f \) is the forward direction voltage of the built-in diode.

Figure 1. Example of a charge-pump-type step-up circuit

Figure 2. Voltages of SW and BOOT
When the SW voltage is low during the switching operations in Figure 2, the electric charge is stored in the capacitor from $V_{IN}$, thus resulting in the voltage of $V_{IN} - V_f$ across the capacitor. When the SW voltage is high, the BOOT voltage increases up to $2 \times V_{IN} - V_f$, and the built-in diode maintains the voltage at $2 \times V_{IN} - V_f$. Therefore, the BOOT voltage switches between $V_{IN} - V_f$ and $2 \times V_{IN} - V_f$ (Figure 3).

![Figure 3. Charge-pump-type step-up circuit diagram](image)

When this BOOT voltage is used as the gate voltage for the high-side N-ch MOSFET, you can obtain a voltage between the gate and the source ($V_{GS}$) that is sufficient to completely turn ON the MOSFET.

In this example, the anode of the built-in diode is obtained from $V_{IN}$, and the BOOT voltage can increase up to $2 \times V_{IN} - V_f$ as described in the calculation. It is possible that this BOOT voltage may exceed the breakdown voltage between the gate and source of the high-side N-ch MOSFET. Therefore, in designing products with a high input voltage, an internal power supply of approximately 5 V is connected to the anode so that the BOOT voltage is maintained below the breakdown voltage between the gate and the source (Figure 4).
3. Capacitance of the bootstrap capacitor

For the minimum capacitance of the bootstrap capacitors, follow the capacitance described in each data sheet. Use a small ceramic capacitor for the bootstrap capacitors. It is necessary to consider the DC bias characteristics of the ceramic capacitors and to confirm that the actual capacitance corresponds with the capacitance described in the data sheet.

The DC bias characteristics refer to the characteristics of variation in capacitance due to the DC voltage applied across the ceramic capacitor. Generally, the capacitance tends to decrease as the DC voltage increases. Furthermore, the variation in capacitance also depends on the size.

Figure 5 shows the examples of DC bias characteristics with different sizes.

When 16 V is applied to the 1005 size ceramic capacitor, the actual capacitance falls significantly below the nominal value of 0.1 μF. Furthermore, approximately half of the nominal value remains. Although the minimum capacitance of the bootstrap capacitor varies with each IC, an excessively small capacitance may result in an electric charge that is insufficient for gate driving. The insufficient electric charge may lead to unstable gate driving and impair the operation.

However, we recommend the use of the minimum capacitor that satisfies the minimum capacitance because a larger size will affect the cost. On the contrary, an excessively large capacitance could delay the increase in the voltage across the capacitor and reduce the voltage for gate driving.

The adequate value of the capacitance can be obtained from the following equations. When the high-side N-ch MOSFET is ON, the electric charge stored in the bootstrap capacitor is consumed for the gate driving.

\[ Q_{LOSS} = Q_G + I_{BOOT} \times D \]

Here, the relation of the variation in the voltage between BOOT and SW (\(\Delta V_{BS}\)), the capacitance of the bootstrap capacitor (\(C_{BOOT}\)), and the \(Q_{LOSS}\) is expressed as follows.

\[ C_{BOOT} \geq \frac{Q_{LOSS}}{\Delta V_{BS}} \]

Considering that it is desirable to maintain \(\Delta V_{BS}\) at 0.1 V or below, the equation can be described as follows.

\[ C_{BOOT} \geq \frac{Q_{LOSS}}{0.1} \]
As an example, a calculation is performed with $Q_G = 10 \text{ nC}$, $I_{BOOBT} = 10 \text{ nA}$, $D = 0.3$, and $f = 1 \text{ MHz}$. From Equation (1),

$$Q_{LOSS} = 10 \text{ nC} + 10 \text{ nA} \times \frac{0.3}{1 \text{ MHz}} \approx 10 \text{ nC}$$

When this value is substituted in Equation (3),

$$C_{BOOT} \geq \frac{10 \text{ nC}}{0.1} = 0.1 \mu\text{F}$$

Therefore, $C_{BOOT}$ should be 0.1 $\mu\text{F}$ or larger.

However, the capacitances described in the data sheet should be used because they are designed according to the results obtained from these equations.

Figure 6. Circuit diagram required for $C_{BOOT}$ determination
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